

# Body-Force Equivalents for Seismic Sources

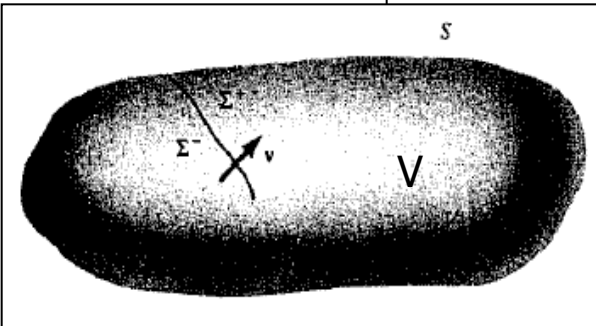
1. Point source representation
2. Body force equivalents
3. Case of a buried fault
4. Seismic Moment

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# Representation Theorem for an Internal Surface

Without assuming any boundary condition on  $\Sigma$ , our first representation theorem reads (repeated):

$$u_n(\mathbf{x}, t) = \int_{-\infty}^{\infty} d\tau \iiint_V f_p(\boldsymbol{\eta}, \tau) G_{np}(\mathbf{x}, t - \tau; \boldsymbol{\eta}, 0) dV(\boldsymbol{\eta}) + \int_{-\infty}^{\infty} d\tau \iint_{\Sigma} \left\{ \left[ u_i(\boldsymbol{\xi}, \tau) c_{ijpq} v_j \frac{\partial G_{np}(\mathbf{x}, t - \tau; \boldsymbol{\xi}, 0)}{\partial \xi_q} - \left[ G_{np}(\mathbf{x}, t - \tau; \boldsymbol{\xi}, 0) T_p(\mathbf{u}(\boldsymbol{\xi}, \tau), \mathbf{v}) \right] \right\} d\Sigma.$$



Suppose that  $\Sigma$  is transparent to  $G$  (i.e.  $G$  satisfies the equation of motion everywhere and is continuous across  $\Sigma$  as well as its derivatives). In the **absence of body forces** for  $u$ , if **slip** arises across  $\Sigma$  then  **$[u]$  is nonzero**, and since **tractions are continuous** across the fault when rupture propagates spontaneously (i.e.  $[T(u, \mathbf{v})] = 0$ ), then

$$u_n(\mathbf{x}, t) = \int_{-\infty}^{\infty} d\tau \iint_{\Sigma} [u_i(\boldsymbol{\xi}, \tau)] c_{ijpq} v_j \frac{\partial}{\partial \xi_q} G_{np}(\mathbf{x}, t - \tau; \boldsymbol{\xi}, 0) d\Sigma.$$

# Representation Theorem for an Internal Surface

Representation Theorem for a Faulting Source (repeated)

$$u_n(\mathbf{x}, t) = \int_{-\infty}^{\infty} d\tau \iint_{\Sigma} [u_i(\boldsymbol{\xi}, \tau)] c_{ijpq} v_j \frac{\partial}{\partial \xi_q} G_{np}(\mathbf{x}, t - \tau; \boldsymbol{\xi}, 0) d\Sigma.$$

This representation formula for displacements, which has been used by many seismologists to evaluate the wavefield radiated from earthquakes, has the following outstanding properties:

1. **Slip** in the fault  $[u_n]$  is enough to determine **displacements everywhere**.
1. **No boundary conditions** on  $\Sigma$  are needed for the **Green function**  $G_{np}$ .
1. **Fault motion**, which may be extremely intricate and may complicate the determination of the slip function  $[u_i(\boldsymbol{\xi}, t)]$ , is completely **independent** from the **Green function** determination.

# Body-Force Equivalents

Making no assumptions about  $[u]$  and  $[T(u,v)]$  across  $\Sigma$ , we have

$$u_n(x, t) = \int_{-\infty}^{\infty} d\tau \iiint_V f_p(\eta, \tau) G_{np}(\mathbf{x}, t - \tau; \eta, 0) dV(\eta) \\ + \int_{-\infty}^{\infty} d\tau \iint_{\Sigma} \left\{ [u_i(\xi, \tau)] c_{ijpq} v_j G_{np,q}(\mathbf{x}, t - \tau; \xi, 0) \right. \\ \left. - [T_p(\mathbf{u}(\xi, \tau), \nu)] G_{np}(\mathbf{x}, t - \tau; \xi, 0) \right\} d\Sigma(\xi).$$

**Traction Discontinuity:** The body-force distribution of a traction discontinuity across  $\Sigma$  is  $[T] \delta(\eta - \xi) d\Sigma$  as  $\eta$  varies throughout  $V$ . Thus, the **contribution to displacement of such a discontinuity** is

$$\int_{-\infty}^{\infty} d\tau \iiint_V \left\{ - \iint_{\Sigma} [T_p(\mathbf{u}(\xi, \tau), \nu)] \delta(\eta - \xi) d\Sigma \right\} G_{np}(\mathbf{x}, t - \tau; \eta, 0) dV.$$

From the representation theorem above we see that the body-force equivalent of a traction discontinuity on  $\Sigma$  is given by  $f^{[T]}$ , where

$$f^{[T]}(\eta, \tau) = - \iint_{\Sigma} [T(\mathbf{u}(\xi, \tau), \nu)] \delta(\eta - \xi) d\Sigma(\xi).$$

# Body-Force Equivalents

$$\begin{aligned}
 u_n(\mathbf{x}, t) = & \int_{-\infty}^{\infty} d\tau \iiint_V f_p(\eta, \tau) G_{np}(\mathbf{x}, t - \tau; \eta, 0) dV(\eta) \\
 & + \int_{-\infty}^{\infty} d\tau \iint_{\Sigma} \left\{ [u_i(\xi, \tau)] c_{ijpq} \nu_j G_{np,q}(\mathbf{x}, t - \tau; \xi, 0) \right. \\
 & \quad \left. - [T_p(\mathbf{u}(\xi, \tau), \nu)] G_{np}(\mathbf{x}, t - \tau; \xi, 0) \right\} d\Sigma(\xi).
 \end{aligned}$$

**Displacement Discontinuity:** We use the following property of the delta-function derivative to localize points of  $\Sigma$  within  $V$ :

$$\frac{\partial}{\partial \xi_q} G_{np}(\mathbf{x}, t - \tau; \xi, 0) = - \iiint_V \frac{\partial}{\partial \eta_q} \delta(\eta - \xi) G_{np}(\mathbf{x}, t - \tau; \eta, 0) dV(\eta),$$

so that the **displacement discontinuity** contributes the displacement with

$$\int_{-\infty}^{\infty} d\tau \iiint_V \left\{ - \iint_{\Sigma} [u_i(\xi, \tau)] c_{ijpq} \nu_j \frac{\partial}{\partial \eta_q} \delta(\eta - \xi) d\Sigma \right\} G_{np}(\mathbf{x}, t - \tau; \eta, 0) dV$$

# Body-Force Equivalents

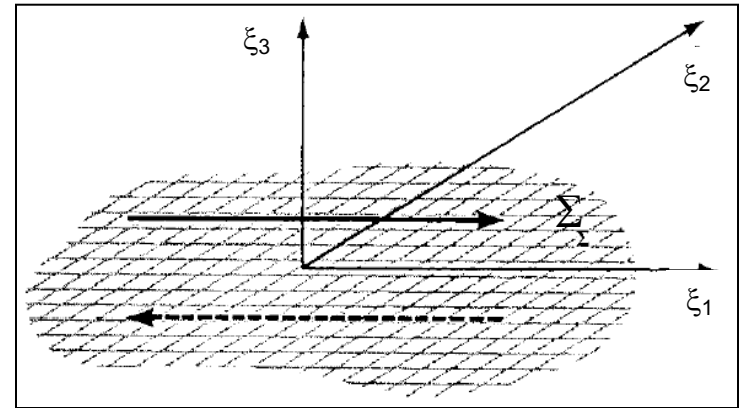
(Displacement Discontinuity)

From the representation theorem before, we see that the **body-force equivalent** of a **displacement discontinuity** on  $\Sigma$  is given by  $f^{[u]}$ , where

$$f_p^{[u]}(\eta, \tau) = - \iint_{\Sigma} [u_i(\xi, \tau)] c_{ijpq} v_j \frac{\partial}{\partial \eta_q} \delta(\eta - \xi) d\Sigma.$$

The **seismic waves** set up by **fault slip** are the same as those set up by a **distribution of certain forces** on the fault with **canceling moment** and **net force**.

The **body-force distribution** is not unique but in an isotropic medium it can always be chosen as a surface distribution of **double couples**.



Assume that the fault  $\Sigma$  lies in the plane  $\xi_3 = 0$  and that the slip  $[u]$  is parallel to the  $\xi_1$ -direction so that  $[u_2] = [u_3] = 0$ . Then the body force equivalent reduces to

$$f_p(\eta, \tau) = - \iint_{\Sigma} [u_1(\xi, \tau)] c_{13pq} \frac{\partial}{\partial \eta_q} \delta(\eta - \xi) d\xi_1 d\xi_2$$

# Body-Force Equivalents

(Displacement Discontinuity)

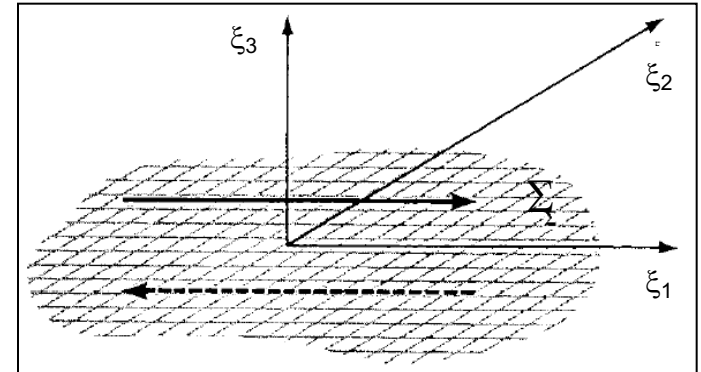
Body force equivalent to the displacement discontinuity shown in the figure below (repeated):

$$f_p(\eta, \tau) = - \iint_{\Sigma} [u_1(\xi, \tau)] c_{13pq} \frac{\partial}{\partial \eta_q} \delta(\eta - \xi) d\xi_1 d\xi_2$$

In isotropic heterogeneous media, from

$$c_{ijkl} = \lambda \delta_{ij} \delta_{kl} + \mu (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk})$$

we find that all  $c_{13pq}$  vanish except  $c_{1313} = c_{1331} = \mu$ . Hence the body-force equivalent distribution over  $\Sigma$  becomes:



$$f_1(\eta, \tau) = - \iint_{\Sigma} \mu(\xi) [u_1(\xi, \tau)] \delta(\eta_1 - \xi_1) \delta(\eta_2 - \xi_2) \frac{\partial}{\partial \eta_3} \delta(\eta_3) d\xi_1 d\xi_2$$

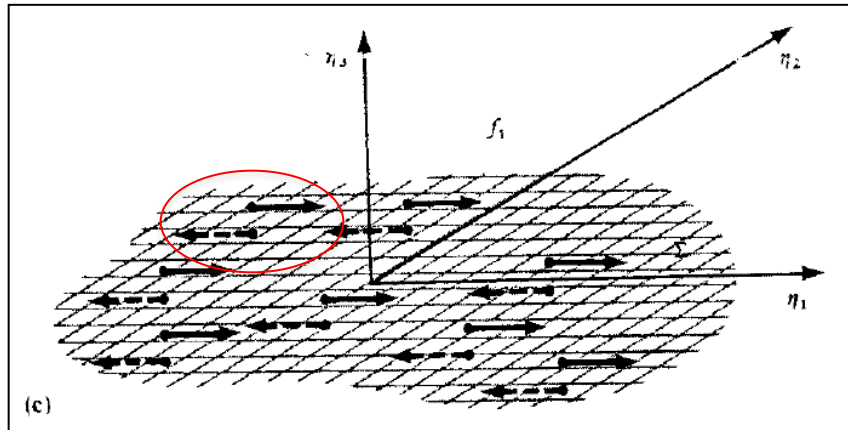
$$f_2(\eta, \tau) = 0,$$

$$f_3(\eta, \tau) = - \iint_{\Sigma} \mu [u_1] \frac{\partial}{\partial \eta_1} \delta(\eta_1 - \xi_1) \delta(\eta_2 - \xi_2) \delta(\eta_3) d\xi_1 d\xi_2.$$

# Force Equivalent for a Buried Fault (Displacement Discontinuity)

Integrating the **first force component** we obtain

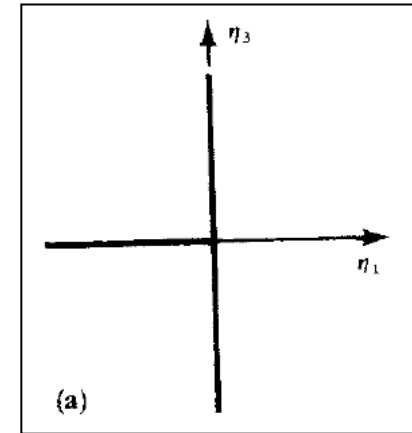
$$f_1(\eta, \tau) = -\mu(\eta) [u_1(\eta, \tau)] \frac{\partial}{\partial \eta_3} \delta(\eta_3)$$



The body force  $(f_1, 0, 0)$  is proportional to the **derivative of the spike** (Dirac) function. It thus represents a system of **single couples** of forces acting in the  $\pm \eta_1$ -direction with **moment along the  $\eta_2$ -direction**. The total moment is not zero and equal to

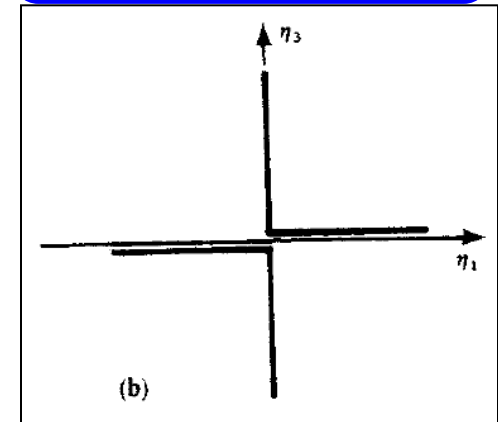
$$\iint_{\Sigma} \mu [u_1(\xi, \tau)] d\Sigma$$

Spike as a function of  $\eta_3$



$$(-\delta(\eta_3), 0, 0)$$

Spike derivative as a function of  $\eta_3$



$$((-\partial/\partial \eta_3)\delta(\eta_3), 0, 0)$$



# Force Equivalent for a Buried Fault (Displacement Discontinuity)

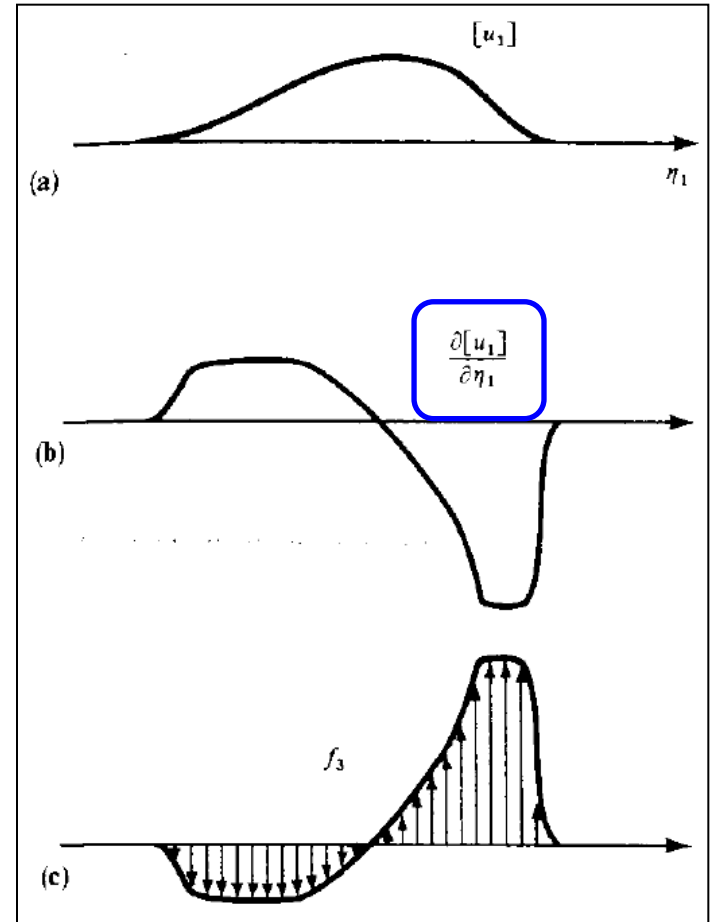
Using properties of the delta derivative, the **third force component** becomes

$$f_3(\eta, \tau) = -\frac{\partial}{\partial \eta_1} \{ \mu [u_1(\eta, \tau)] \} \delta(\eta_3).$$

The body force  $(0,0,f_3)$  is a **single force** proportional to the **derivative of the slip function**. It thus represents a force distribution in the **+/-  $\eta_3$ -direction** yielding a net couple with **moment along the  $-\eta_2$ -direction**. The total moment is not zero and equal to

$$-\iint_{\Sigma} \mu [u_1] d\xi_1 d\xi_2.$$

which is the same, but with opposite sign, as the total moment due to the force equivalent  $f_1$ . It can be shown that such moment is given by  $\mu \bar{u} A$  where  $A$  is the total fault area. **Moments from both body-force equivalents cancel out.**



# Force Equivalent for a Buried Fault (Displacement Discontinuity)

Body force equivalents to a given fault slip **are not unique**. The single force distribution  $f_3$  shown in last figure is also equivalent to a distribution of single couples. To see this, take the representation

$$u_n(\mathbf{x}, t) = \int_{-\infty}^{\infty} d\tau \iint_{\Sigma} [u_i(\boldsymbol{\xi}, \tau)] c_{ijpq} \nu_j \frac{\partial}{\partial \xi_q} G_{np}(\mathbf{x}, t - \tau; \boldsymbol{\xi}, 0) d\Sigma.$$

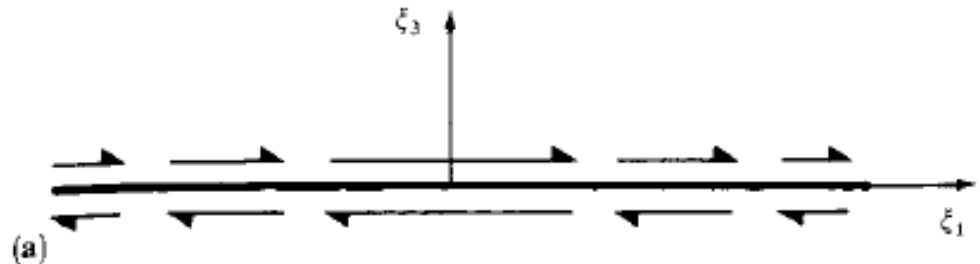
and particularize it for the chosen fault plane and slip direction:

$$u_n(\mathbf{x}, t) = \int_{-\infty}^{\infty} d\tau \iint_{\Sigma} \mu [u_1] \left\{ \frac{\partial G_{n1}}{\partial \xi_3} + \frac{\partial G_{n3}}{\partial \xi_1} \right\} d\Sigma.$$

The first term in the curl brackets is the limit

$$\frac{G_{n1}(\mathbf{x}, t - \tau; \boldsymbol{\xi} + \varepsilon \hat{\xi}_3, 0) - G_{n1}(\mathbf{x}, t - \tau; \boldsymbol{\xi} - \varepsilon \hat{\xi}_3, 0)}{2\varepsilon}$$

as  $\varepsilon \rightarrow 0$ . This is the following single-couple distribution (notice the moment units, **Nw\*m**, of the equation):

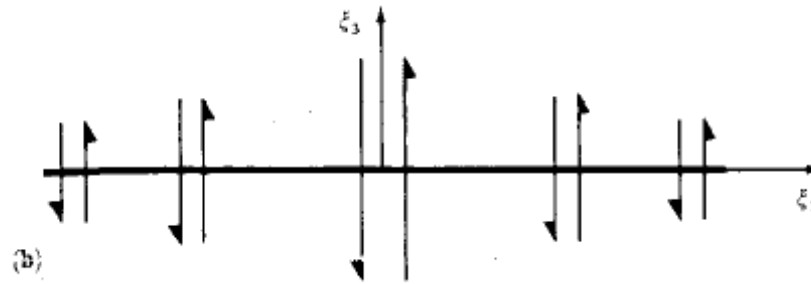


# Force Equivalent for a Buried Fault (Displacement Discontinuity)

The second term involves the limit

$$\frac{G_{n3}(\mathbf{x}, t - \tau; \xi + \varepsilon \hat{\xi}_1, 0) - G_{n3}(\mathbf{x}, t - \tau; \xi - \varepsilon \hat{\xi}_1, 0)}{2\varepsilon},$$

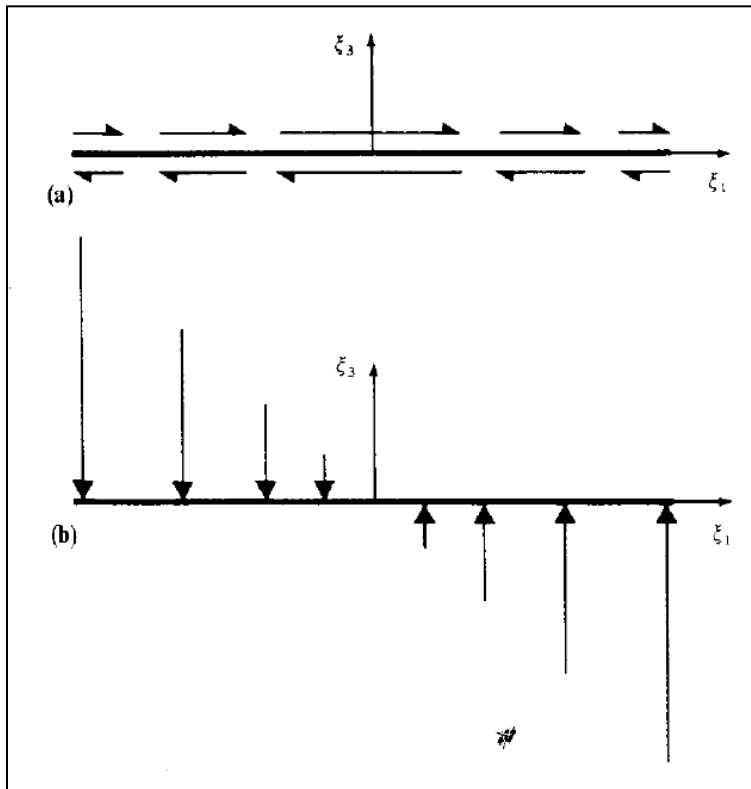
as  $\varepsilon \rightarrow 0$ , which represents the following single-couple distribution:



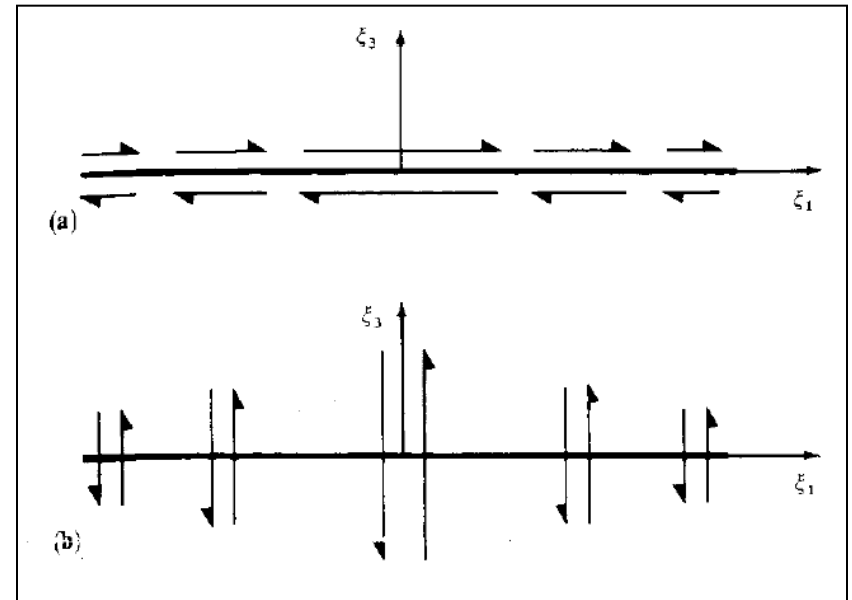
# Force Equivalent for a Buried Fault

The complete **body-force equivalent** to **fault slip** consists of **two parts** with both canceling moment and net force:

1. **Single couples** ( $f_1$ ) made up of forces pointing in the fault slip direction, and
2. A **distribution of a fault-normal single forces** over  $\Sigma$  ( $f_3$ ) with total moment cancelling the one due to  $f_1$ .



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# Force Equivalent for a Buried Fault

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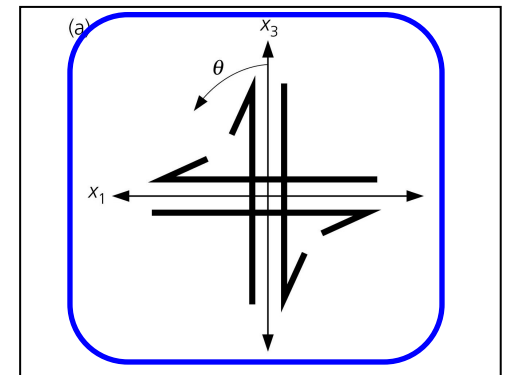
The absolute value of the total moment associated with each contribution is equal to  $\boxed{\mu \bar{u} A}$

At **great distances from the fault**, wavelengths of seismic waves are much greater than the linear dimension of  $\Sigma$ , and their periods much longer than the source duration. **The slip thus becomes localized in space and time**  $\boxed{\bar{u} A \delta(\xi_1) \delta(\xi_2) H(\tau)}$  and then:

$$f_1(\eta, \tau) = -M_0 \delta(\eta_1) \delta(\eta_2) \frac{\partial}{\partial \eta_3} \delta(\eta_3) H(\tau)$$

$$f_3(\eta, \tau) = -M_0 \frac{\partial}{\partial \eta_1} \delta(\eta_1) \delta(\eta_2) \delta(\eta_3) H(\tau)$$

**Double Couple:** Point dislocation body-force equivalent



where  $M_0$  is called the **seismic moment**:

$$M_0 = \mu \bar{u} A = \mu \times \text{average slip} \times \text{fault area.}$$